

A2.04	PREDNÁŠKOVÁ SÁLA	63,59				ČAS	8	9	10	11	12	13	14	15	16	37	2,96	4,22	7,28
			S	9,75	0,15	$I_{OS} [W.m^{-2}]$	100	117	130	139	141	139	130	117	100				
						$I_{DS} = A_S \cdot I_{OS} \cdot s [W]$	97,50	114,08	126,75	135,53	137,48	135,53	126,75	114,08	97,50				
			J	-	-	$I_{OJ} [W.m^{-2}]$	128	230	335	409	435	409	335	230	128				
						$I_{DJ} = A_J \cdot I_{OJ} \cdot s [W]$	0	0	0	0	0	0	0	0	0				
			V	-	-	$I_{OV} [W.m^{-2}]$	539	505	389	232	141	139	130	117	100				
						$I_{DV} = A_V \cdot I_{OV} \cdot s [W]$	0	0	0	0	0	0	0	0	0				
			Z	-	-	$I_{OZ} [W.m^{-2}]$	100	117	130	139	141	232	389	505	539				
						$I_{DZ} = A_Z \cdot I_{OZ} \cdot s [W]$	0	0	0	0	0	0	0	0	0				
			H	-	-	$I_{OH} [W.m^{-2}]$	379	534	640	706	729	706	640	534	397				
						$I_{DH} = A_H \cdot I_{OH} \cdot s [W]$	0	0	0	0	0	0	0	0	0				
			$\Sigma I_D = Q_W$	97,50	114,08	126,75	135,53	137,48	135,53	126,75	114,08	97,50							
																			79,29

BLOK B - KANCELÁRIE

VÝPOČET TEPELNEJ ZÁŤAŽE OD RADIÁCIE OKNAMI, OSÔB A TECHNOLOGICKÝCH ZARIADENÍ																			
Č. M.	ÚČEL MIESTNOSTI	PLOCHA [m ²]	FASÁDA	PLOCHA OKIEN A [m ²]	SÚČINITEL' ZATIENENIA s [-]	VÝPOČET TEPELNEJ ZÁŤAŽE OKIEN RADIÁCIOU - Q _W [W]										POČET OSÔB	Q ₀ - ZÁŤAŽ OSOBAMI (80 W/os.) [kW]	Q _{TECH} - ZÁŤAŽ TECH. ZARIADENÍ A OSVETLENÍM [kW]	TEPELNÁ ZÁŤAŽ Q ₁ = Q _W +Q ₀ +Q _{TECH} [kW]
B1.18	KANCELÁRIA	18,36				ČAS	8	9	10	11	12	13	14	15	16	1	0,08	0,29	0,58
			S	9,80	0,15	I _{OS} [W.m ⁻²]	100	117	130	139	141	139	130	117	100				
						I _{DS} = A _S ·I _{OS} ·s [W]	147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00				
			J	-	-	I _{OJ} [W.m ⁻²]	128	230	335	409	435	409	335	230	128				
						I _{DJ} = A _J ·I _{OJ} ·s [W]	0	0	0	0	0	0	0	0	0				
			V	-	-	I _{OV} [W.m ⁻²]	539	505	389	232	141	139	130	117	100				
						I _{DV} = A _V ·I _{OV} ·s [W]	0	0	0	0	0	0	0	0	0				
			Z	-	-	I _{OZ} [W.m ⁻²]	100	117	130	139	141	232	389	505	539				
						I _{DZ} = A _Z ·I _{OZ} ·s [W]	0	0	0	0	0	0	0	0	0				
			H	-	-	I _{OH} [W.m ⁻²]	379	534	640	706	729	706	640	534	397				
I _{DH} = A _H ·I _{OH} ·s [W]	0	0				0	0	0	0	0	0	0							
ΣI _D = Q _W						147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00					
B1.19	KANCELÁRIA	17,63				ČAS	8	9	10	11	12	13	14	15	16	1	0,08	0,29	0,58
			S	9,80	0,15	I _{OS} [W.m ⁻²]	100	117	130	139	141	139	130	117	100				
						I _{DS} = A _S ·I _{OS} ·s [W]	147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00				
			J	-	-	I _{OJ} [W.m ⁻²]	128	230	335	409	435	409	335	230	128				
						I _{DJ} = A _J ·I _{OJ} ·s [W]	0	0	0	0	0	0	0	0	0				
			V	-	-	I _{OV} [W.m ⁻²]	539	505	389	232	141	139	130	117	100				
						I _{DV} = A _V ·I _{OV} ·s [W]	0	0	0	0	0	0	0	0	0				
			Z	-	-	I _{OZ} [W.m ⁻²]	100	117	130	139	141	232	389	505	539				
						I _{DZ} = A _Z ·I _{OZ} ·s [W]	0	0	0	0	0	0	0	0	0				
			H	-	-	I _{OH} [W.m ⁻²]	379	534	640	706	729	706	640	534	397				
I _{DH} = A _H ·I _{OH} ·s [W]	0	0				0	0	0	0	0	0	0							
ΣI _D = Q _W						147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00					
B1.20	KANCELÁRIA	17,63				ČAS	8	9	10	11	12	13	14	15	16	1	0,08	0,29	0,58
			S	9,80	0,15	I _{OS} [W.m ⁻²]	100	117	130	139	141	139	130	117	100				
						I _{DS} = A _S ·I _{OS} ·s [W]	147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00				
			J	-	-	I _{OJ} [W.m ⁻²]	128	230	335	409	435	409	335	230	128				
						I _{DJ} = A _J ·I _{OJ} ·s [W]	0	0	0	0	0	0	0	0	0				
			V	-	-	I _{OV} [W.m ⁻²]	539	505	389	232	141	139	130	117	100				
						I _{DV} = A _V ·I _{OV} ·s [W]	0	0	0	0	0	0	0	0	0				
			Z	-	-	I _{OZ} [W.m ⁻²]	100	117	130	139	141	232	389	505	539				
						I _{DZ} = A _Z ·I _{OZ} ·s [W]	0	0	0	0	0	0	0	0	0				
			H	-	-	I _{OH} [W.m ⁻²]	379	534	640	706	729	706	640	534	397				
I _{DH} = A _H ·I _{OH} ·s [W]	0	0				0	0	0	0	0	0	0							
ΣI _D = Q _W						147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00					
B1.21	KANCELÁRIA	19,67				ČAS	8	9	10	11	12	13	14	15	16	1	0,08	0,30	0,59
			S	9,80	0,15	I _{OS} [W.m ⁻²]	100	117	130	139	141	139	130	117	100				
						I _{DS} = A _S ·I _{OS} ·s [W]	147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00				
			J	-	-	I _{OJ} [W.m ⁻²]	128	230	335	409	435	409	335	230	128				
						I _{DJ} = A _J ·I _{OJ} ·s [W]	0	0	0	0	0	0	0	0	0				
			V	-	-	I _{OV} [W.m ⁻²]	539	505	389	232	141	139	130	117	100				
						I _{DV} = A _V ·I _{OV} ·s [W]	0	0	0	0	0	0	0	0	0				
			Z	-	-	I _{OZ} [W.m ⁻²]	100	117	130	139	141	232	389	505	539				
						I _{DZ} = A _Z ·I _{OZ} ·s [W]	0	0	0	0	0	0	0	0	0				
			H	-	-	I _{OH} [W.m ⁻²]	379	534	640	706	729	706	640	534	397				
I _{DH} = A _H ·I _{OH} ·s [W]	0	0				0	0	0	0	0	0	0							
ΣI _D = Q _W						147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00					
B1.22	KANCELÁRIA	19,67				ČAS	8	9	10	11	12	13	14	15	16	1	0,08	0,30	0,59
			S	9,80	0,15	I _{OS} [W.m ⁻²]	100	117	130	139	141	139	130	117	100				
						I _{DS} = A _S ·I _{OS} ·s [W]	147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00				
			J	-	-	I _{OJ} [W.m ⁻²]	128	230	335	409	435	409	335	230	128				
						I _{DJ} = A _J ·I _{OJ} ·s [W]	0	0	0	0	0	0	0	0	0				
			V	-	-	I _{OV} [W.m ⁻²]	539	505	389	232	141	139	130	117	100				
						I _{DV} = A _V ·I _{OV} ·s [W]	0	0	0	0	0	0	0	0	0				
			Z	-	-	I _{OZ} [W.m ⁻²]	100	117	130	139	141	232	389	505	539				
						I _{DZ} = A _Z ·I _{OZ} ·s [W]	0	0	0	0	0	0	0	0	0				
			H	-	-	I _{OH} [W.m ⁻²]	379	534	640	706	729	706	640	534	397				
I _{DH} = A _H ·I _{OH} ·s [W]	0	0				0	0	0	0	0	0	0							
ΣI _D = Q _W						147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00					
B1.23	KANCELÁRIA	17,66				ČAS	8	9	10	11	12	13	14	15	16	1	0,08	0,29	0,58
			S	9,80	0,15	I _{OS} [W.m ⁻²]	100	117	130	139	141	139	130	117	100				
						I _{DS} = A _S ·I _{OS} ·s [W]	147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00				
			J	-	-	I _{OJ} [W.m ⁻²]	128	230	335	409	435	409	335	230	128				
						I _{DJ} = A _J ·I _{OJ} ·s [W]	0	0	0	0	0	0	0	0	0				
			V	-	-	I _{OV} [W.m ⁻²]	539	505	389	232	141	139	130	117	100				
						I _{DV} = A _V ·I _{OV} ·s [W]	0	0	0	0	0	0	0	0	0				
			Z	-	-	I _{OZ} [W.m ⁻²]	100	117	130	139	141	232	389	505	539				
						I _{DZ} = A _Z ·I _{OZ} ·s [W]	0	0	0	0	0	0	0	0	0				
			H	-	-	I _{OH} [W.m ⁻²]	379	534	640	706	729	706	640	534	397				
I _{DH} = A _H ·I _{OH} ·s [W]	0	0				0	0	0	0	0	0	0							
ΣI _D = Q _W						147,00	171,99	191,10	204,33	207,27	204,33	191,10	171,99	147,00					